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Status and plans of mechanical analysis of different 2nd generation IR quad designs

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OUTLINE:

- ❖ Goal and plans
- ❖ Where we are now
- ❖ Next steps



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Goal and plans

- GOALS:**
- Study and compare mechanical designs for both shell and racetrack type quadrupoles in order to select the best design concept for the 1st short model,
 - Have engineering design by the end of FY05.

- Candidates:**
- Shell type $\phi = 110$ mm with Aluminum outer shell
 - Shell type $\phi = 110$ mm with Stainless Steel skin
 - Racetrack type $\phi = 92$ mm with Al/SS skin

- Criteria:**
- Acceptable stress and strain in the coil
 - Acceptable coil deformation

- STEPS:**
- Analytical analysis
 - FEM with fixed BC
 - FEM with external forces
 - Full FEM model (conceptual)



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Shell type – Magnetic forces

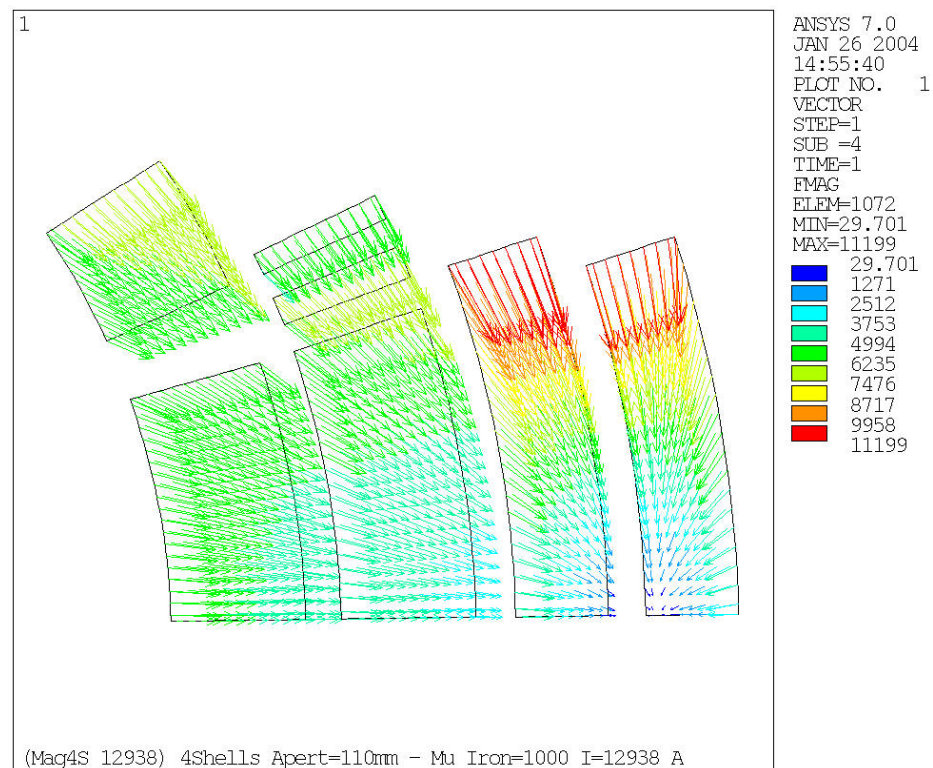


❖ **Forces computed by
ROXIE and ANSYS**

@ I=13kA (= 228 T/m)

	ROXIE (MN/m)	ANSYS (MN/m)	HGQ† (MN/m)
F_X	4.2	4.2	1.6
F_Y	-4.2	-4.1	-1.9
F_R		2.8	
F_θ		-5	

† KEK design scaled to 228 T/m





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Shell type – Analytical study



❖ **1st shell: $F_{\theta} = 1.5 \text{ MN/m}$,**

○ **Width = 12.3 mm,**

➔ **$\sigma_{\theta} = 122 \text{ MPa}$**

❖ **Bottom half of coil: $F_r = 1.7 \text{ MN/m}$,**

○ **$E_{r_coil} = 50 \text{ GPa}$, $E_{r_ins} = 14 \text{ GPa}$**

➔ **$\Delta r = 87 \text{ }\mu\text{m}$ (average)**

And this deflection is going to increase the stress in the 1st shell!



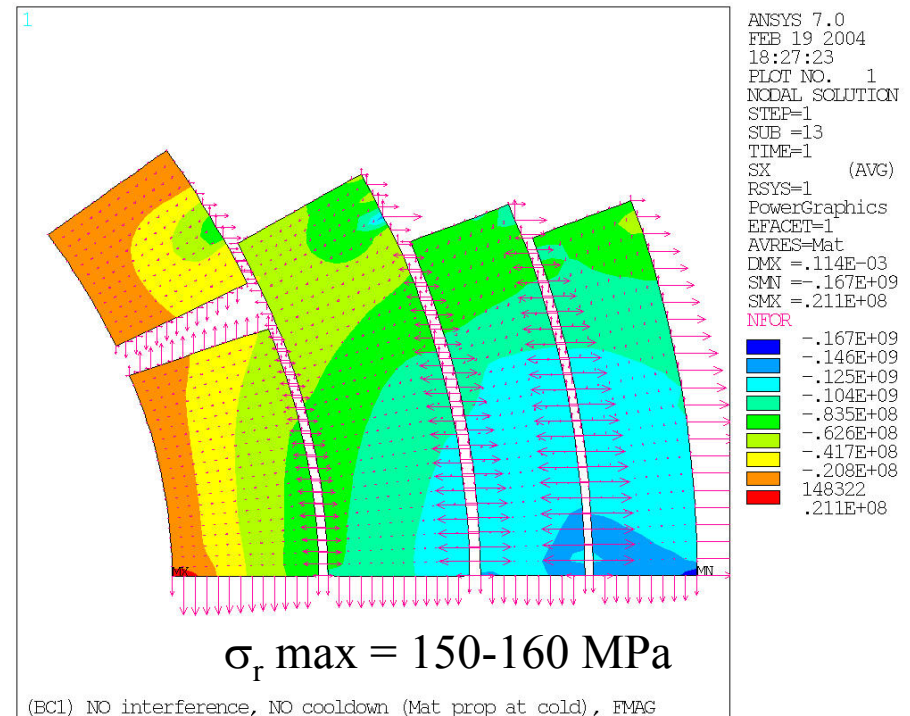
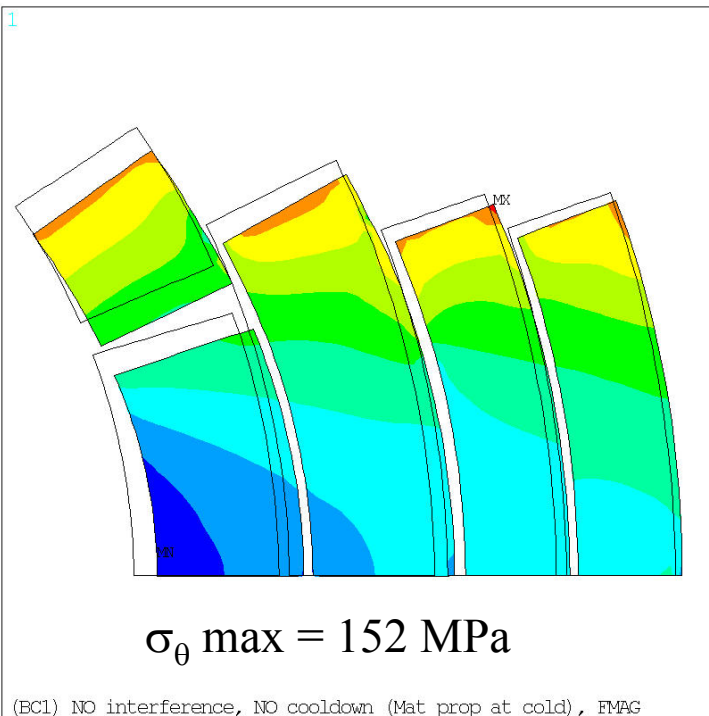
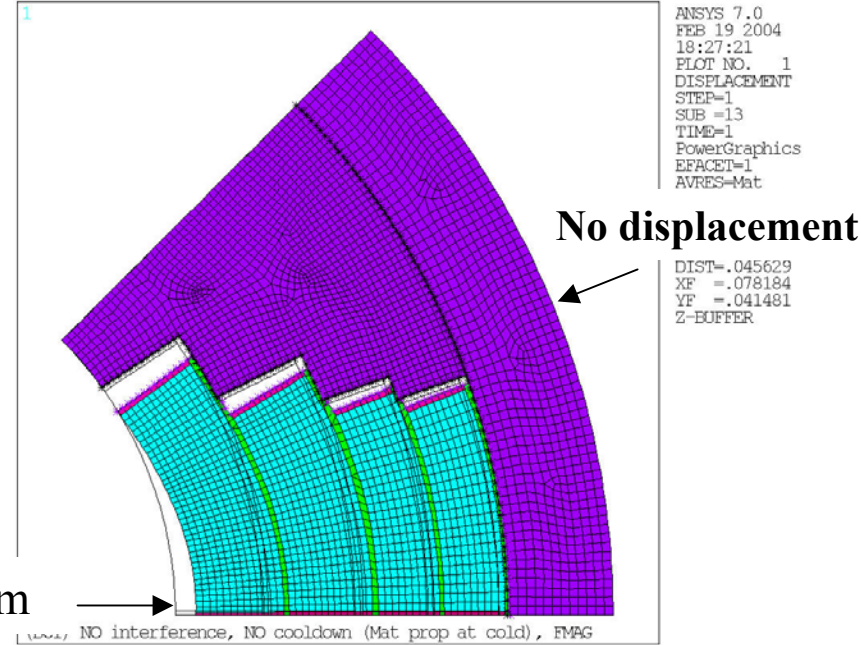
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Shell type Infinitely rigid B.C.

❖ Stress in the coil with infinitely rigid BC on the outer surface of the collars

- NO pre-stress
- Material properties @ 4.2 K
- Fmag @ 13 kA = 228 T/m

$$\Delta r = 87 \mu\text{m}$$



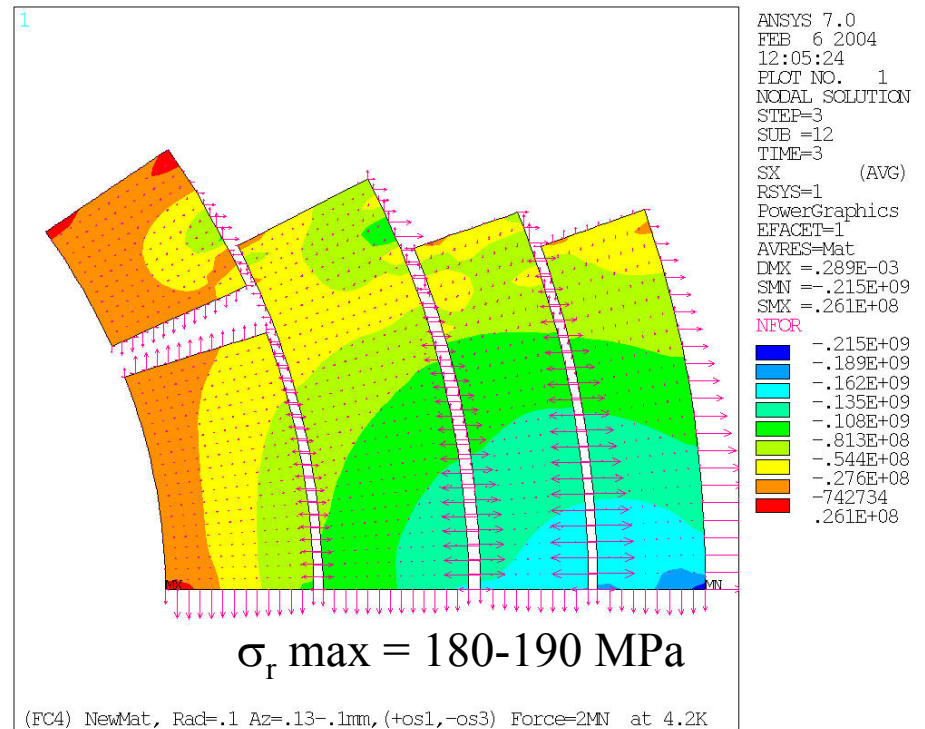
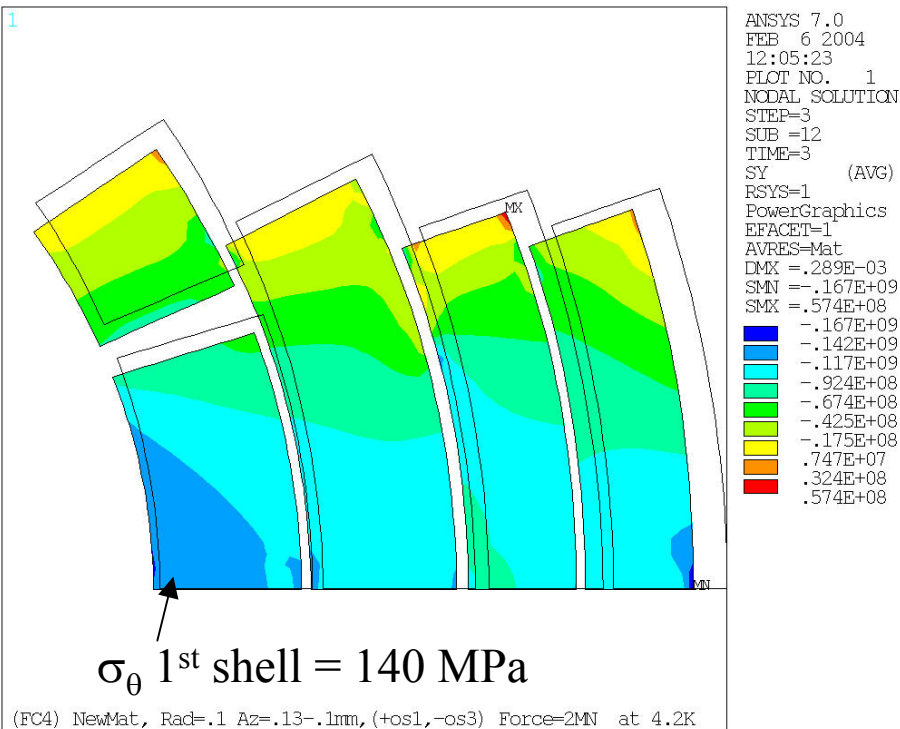
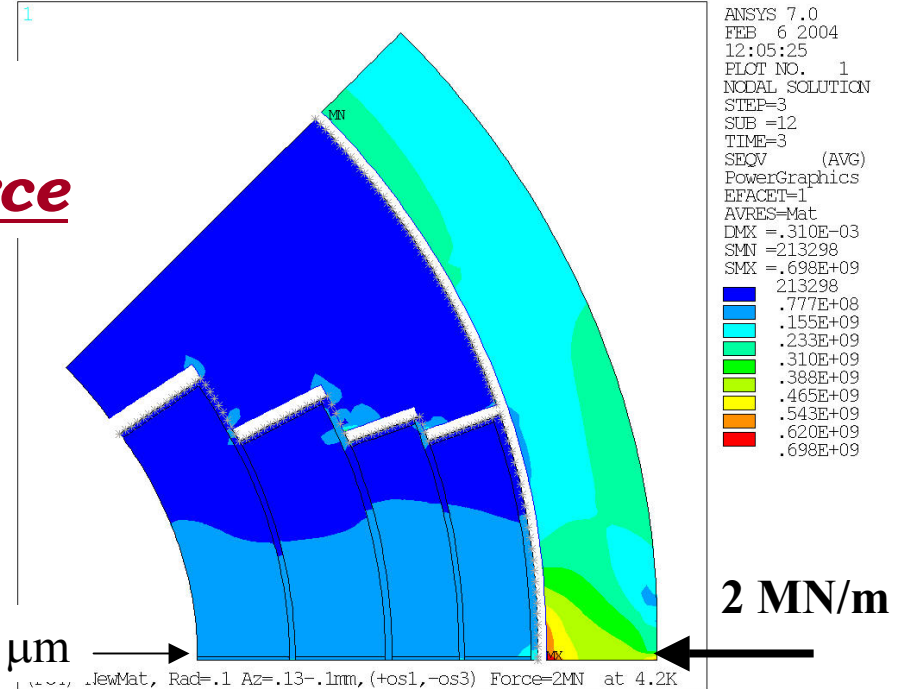


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Shell type FEM with external force

❖ Stress in the coil with horizontal force on the midplane

- With some pre-stress <120 MPa
- $F_{mag} @ 13 \text{ kA} = 228 \text{ T/m}$

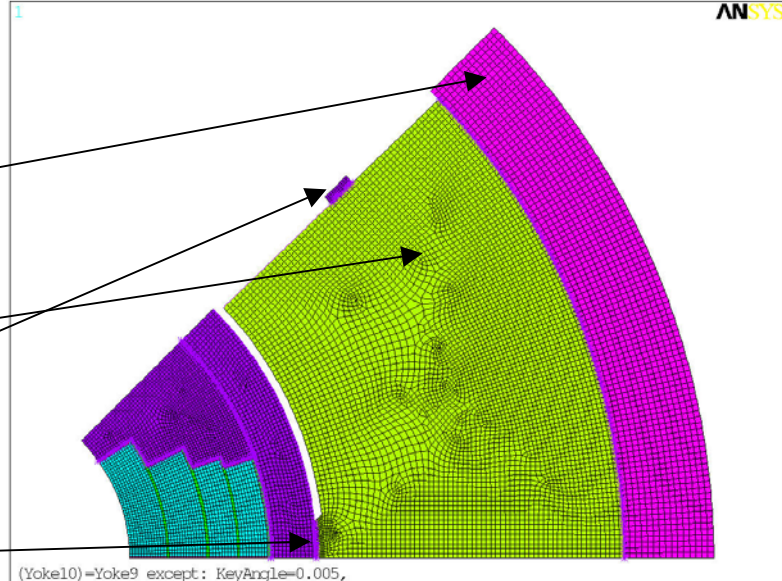




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Shell type with Al outer shell

- ❖ Al shell
- ❖ Yoke with gap at 45 deg.
- ❖ SS keys in contact after cooldown and at max Grad.
- ❖ Collar-Yoke contact 0-6 deg.
- ❖ Bladder technology



σ_θ at 228 T/m

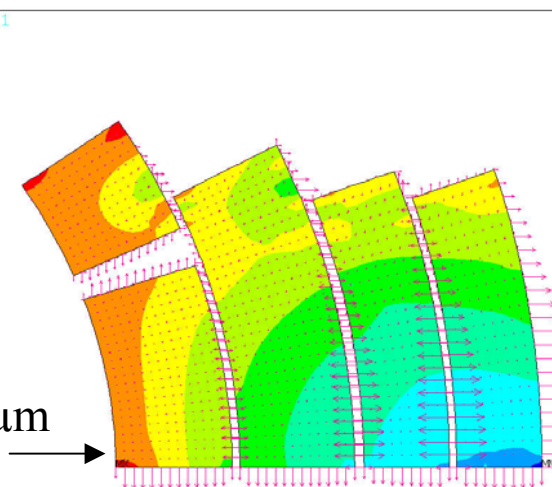
Tops of shells are still in contact



ANSYS 7.0
FEB 23 2004
16:12:25
PLOT NO. 1
NODAL SOLUTION
STEP=3
SUB =12
TIME=3
SY (AVG)
RSYS=1
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.302E-03
SMN =-.172E+09
SMX =.565E+08
-.169E+09
-.148E+09
-.127E+09
-.106E+09
-.850E+08
-.640E+08
-.430E+08
-.220E+08
-.100E+07
.200E+08

σ_r at 228 T/m

$\Delta r = 131 \mu\text{m}$



$\sigma_r \text{ max} = 160-180 \text{ MPa}$

ANSYS 7.0
FEB 23 2004
14:44:59
PLOT NO. 1
NODAL SOLUTION
STEP=3
SUB =12
TIME=3
SX (AVG)
RSYS=1
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.302E-03
SMN =-.207E+09
SMX =.245E+08
NECR
-.207E+09
-.181E+09
-.155E+09
-.130E+09
-.104E+09
-.783E+08
-.526E+08
-.269E+08
-.119E+07
.245E+08

(Yoke10)=Yoke9 except: KeyAngle=0.005,



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Next steps



❖ Shell type with SS skin

By the end of Q2

❖ Block type ($F_x=5.5$ $F_y=-6$ MN/m @ 228 T/m)

By the end of Q3

- Analytical study
- FEM with fixed BC
- FEM with external help (force and/or BC)
- Full FE model (conceptual)
- Comparison with LBNL design

❖ Sensitivity analysis

By the end of FY04

- As part of the decision process

Decision for 1st short model

❖ Final design of 1st short model with magnetic and mechanical optimization

By the end of FY05